Operation Reliability and Diagnostics of Mechanical Systems via RDIS Application

Jiří Stodola & Petr Stodola University of Defense Brno





1. INTRODUCTION - RDIS

- diagnostic parameters, physical methods of diagnostics used, methods, methodologies, sensors, diagnostic signals, etc.,
- determination and characteristics of operating mode (continuous, cyclic, operating, general),
- technique of failure data collection in time (time protocol, formalized documents, automatic data collection, coding, classification, filtering, security, etc.),

1. INTRODUCTION - RDIS

- methodology and analysis of information obtained (software, routine and special outputs, etc.),
- additional information or necessary experiments to explain complex outputs,
- elasticity, effectiveness, integrity, efficiency, compatibility (Microsoft Office, etc.), reliability (ISO 9001), periodical updating, open (modular) design, superstructure availability, departmental solution, etc.



Block diagram of information about failure rate and corrective measures



Input information for the analysis of mechanical systems reliability can be presented as a set of vectors: v_i, n_v(T), t_{vi}(T) and r_{vi}, for which it is valid

$$\mathbf{v}_i = [\mathbf{v}_1, \, \mathbf{v}_2, \, \dots \, \mathbf{v}_i, \dots, \, \mathbf{v}_k] \,,$$
 (1)

$$n_{v}(T) = [n_{v1}, n_{v2}, \dots, n_{vi}, \dots, n_{vk}],$$
 (2)

$$t_{vi}(T) = [t_{vi}(1), t_{vi}(2), .., t_{vi}(i), .., t_{vi}(k)]$$
(3)

$$r_{vi} = [r_{v1}, r_{v2}, \dots, r_{vi}, \dots, r_{vk}], \qquad (4)$$

There are many methodologies and assessment to analyze data on mechanical systems, for example:

- Wöhler or Weibull fatigue tests,
- Simultaneous fatigue tests,
- Censured fatigue tests according to time or samples,
- Probability models,
- Approximative models,
- Correlation analysis,
- Testing procedures, etc.

An appropriate method is a correlation analysis related to the vector $n_v(T)$;

$$\mathbf{n}(v_i, v_j) = \begin{vmatrix} n_{11} & n_{12} & \dots & n_{1j} & \dots & n_{1k} \\ n_{21} & n_{22} & \dots & n_{2j} & \dots & n_{2k} \\ \vdots & \vdots & \ddots & \ddots & \ddots & \vdots \\ n_{i1} & n_{i2} & \dots & n_{ij} & \dots & n_{ik} \\ \vdots & \vdots & \dots & \vdots & \ddots & \vdots \\ n_{k1} & n_{k2} & \dots & n_{kj} & \dots & n_{kk} \end{vmatrix}$$

Where diagonal elements n_{ii} for i = 1, 2, ..., k, determine the rate of independently occurring failures, and present simultaneously generated failures. It is valid failure rate, type v_i for i = 1, 2, ..., k,

$$\sum_{j=1}^{k} n_{ij} = n_{vi} = n_{ij}$$

It is valid failure rate, type v_j for j = 1, 2, ..., k,

$$\sum_{i=1}^{k} n_{ij} = n_{vj} = n_j$$

It is valid number of all failures, type v_i and v_i ∩ v_j, for *i*, *j* = 1, 2, ..., *k*, within the interval <0, *T*>;

$$\sum_{i=1}^{k} \sum_{j=1}^{k} n_{ij} = n(T)$$

 $n_{ij} = n(v_i, v_j)$... failure rate, type v_i and v_j produced simultaneously,

The matrix of relative failure rates is defined

 $\begin{bmatrix} p(v_i, v_j) \end{bmatrix} = \begin{bmatrix} p_1(1) & p_2(1) & \dots & p_j(1) & \dots & p_k(1) \\ p_1(2) & P_2(2) & \dots & p_j(2) & \dots & p_k(2) \\ & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots \\ p_1(i) & p_2(i) & \dots & p_j(i) & \dots & p_k(i) \\ & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots \\ p_1(k) & p_2(k) & \dots & p_j(k) & \dots & p_k(k) \end{bmatrix}$

Thus, it will hold

$$\sum_{j=1}^{k} p_{j}(i) = \sum_{i=1}^{k} p_{j}(i) = 1$$

where p_j(i) ... probability of simultaneous failures v_i and v_i.

If n₁, n₂, ..., n_k are non-negative integer numbers and if it holds that, then we shall expect n₁, n₂, ..., n_k in multinonic distribution with a probability

$$P(n_1, n_2, \dots, n_k) = \frac{n!}{n_1! n_2! \dots n_k!} \pi_1^{n_1} \pi_2^{n_2} \dots \pi_k^{n_k}$$

The distribution function of multinonic distribution of simultaneous occurrence of various types of failures provides to calculate strength of a possible stochastic dependence between them – the correlation coefficient

$$r_{ij} = -\sqrt{\frac{p_i(i).p_j(i)}{[1 - p_i(i)][1 - p_j(i)]}}$$

RDIS included a study of operation failures of connecting-rod sliding bearings of the internal combustion engines.







It referred to 7 connecting-rod sliding bearings, the failures of which were caused by the following 11 wear mechanisms. These are:

- **Adhesion**, vector $-v_1$,
- Abrasion (knurling, cutting), vector v_2 ,
- Erosion, vector v_3 ,
- Fatigue, vector v_4 ,
- **Vibrations**, vector $-v_5$,
- **Cavitation**, vector $-v_6$,
 - Mixture, vector *v*₇,

- **Peeling off the surface, vector** $-v_8$,
- **Corrosion**, vector $-v_9$,
- Mechanisms of failures caused by changes of geometric shape (ovality, conicity, etc.), vector – v₁₀,
- Mechanisms of failures caused by operating (technological or installation), vector v₁₁.

Products of wear process



◄ Abrasion particles



◄ Sferoids

▼ Syntetic fibres













3. APPLICATION- crankcase



3. APPLICATION Piston, piston pin, piston ring, connecting rod

3. APPLICATION - connecting rod screw



For all mentioned mechanisms, typical characteristics (number, shape and size of wear particles, morphology of wear particle surface and worn bearing, etc.) were determined; standards, gauges and decision criteria for assessment of a technical condition in dependence on performance parameter (number of kilometers covered, number of hours worked Mh, fuel consumed, physical age, etc.) were stated.

The result of study was to approximately assess a residual life and prevailing mechanism of wear, vector – v_i for i = 1, 2,..., 11. Further solution consisted in identification of 35 basic features (Z₁ – Z₃₅), obtained by diagnostics of engines in view, specification of which can be seen in Tab. 1.

Simple correlation analysis of featured pairs resulted in the matrix correlation coefficients in the form

$$\begin{bmatrix} r(Z_i, Z_j) \end{bmatrix} = \begin{bmatrix} 1 & r_{12} & \dots & r_{1j} & \dots & r_{1,35} \\ r_{21} & 1 & \dots & r_{2j} & \dots & r_{2,35} \\ \vdots & \vdots & \ddots & \ddots & \vdots & \vdots \\ r_{i1} & r_{i,2} & \dots & r_{ij} & \dots & r_{i,35} \\ \vdots & \vdots & \ddots & \ddots & \vdots & \vdots \\ r_{35,1} & r_{35,2} & \dots & r_{35,j} & \dots & 1 \end{bmatrix}$$



4. CONCLUSION

For an actual given example, cases were analyzed when a time of operation (feature Z₃) is significantly stochastically dependent on further features Z_i. In practice, it was the analysis of features (Z₃, Z_i) for i = 7, 8, 10, 23, at which an important correlation dependency was observed, in the following order

$$\{Z_3 \leftrightarrow Z_8\} \quad \dots \quad r_{3,8} = 0.84 ; \quad d_{3,8} = 71 \%$$

$$\{Z_3 \leftrightarrow Z_7\} \quad \dots \quad r_{3,7} = 0.70 ; \quad d_{3,7} = 50 \%$$

$$\{Z_3 \leftrightarrow Z_{23}\} \quad \dots \quad r_{3,23} = 0.68 ; \quad d_{3,23} = 46 \%$$

$$\{Z_3 \leftrightarrow Z_{10}\} \quad \dots \quad r_{3,10} = 0.62 ; \quad d_{3,10} = 38 \%$$

4. CONCLUSION

- These will be the following close relations:
- Time of operation smooth wear of the center of sliding surfaces,
- Time of operation smooth wear of the edges of sliding surfaces,
- Time of operation friction corrosion of external surfaces,
- Time of operation stains on sliding surfaces;

4. CONCLUSION

The result of research provides important information enabling optimizing the operating diagnostics of objects tested (internal combustion engines) based on five important diagnostic parameters.

